



# MOX@EON

## EON Operational Experience

Fall 2011 Meeting of the  
US Nuclear Waste Technical Review  
Board

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# Irradiation Record of EON-NPPs

NPPs	HM U-FA (t)	Reproc. (t)	HM MOX (t)	Pu (t)
Brokdorf	609	187	126	8
Unterweser	839	517	107	6
Grohnde	739	283	66	4
Grafenrheinfeld	793	376	81	5
Isar-2	603	181	81	5
Stade	496	496	0	0
Würgassen	344	344	0	0
Isar-1	733	337	0	0
total	5155	2721	461	28
Pu	57	Pu for EKK		

MOX still to be loaded: 88 PWR/47 t HM/3 t Pu

## Balance for EKK operated units (8)

5200 t HM in U-FA irradiated  
2700 t HM reprocessed (50%)

60 t Pu created

30 t (50%) recycled as MOX



# MOX Licensing at EKK units (authorities of 3 different states)

	MOX / reload	MOX / core	Pufiss/Putot	Pufiss	U-235	remark
KBR	1/3	64	equivalent to 4,0w/o U-235		Unat Utails	no. enr-levels not restricted, wet storage
KKU	16/20/24 (59/71/>71)	96	<= 81,4	3,5 4,5	Unat Utails	16x16-20-4; 3 enr.-levels; wet storage
KWG	16	64		3,2	Unat	16x16-20-4; wet storage only
KKG	16	64	81,4 58...71 <sup>1)</sup>	3,07 4,65	Unat Utails <sup>2)</sup>	no. enr-levels not restricted, wet storage
KKI-2	24	96	71,2 equivalent to 4,4 w/o U-235	3,8	Unat Utails	18x18-24-4, no. enr-levels not restricted, wet storage
KKS	n.a.	n.a.	n.a.	n.a.	n.a.	
KWW	n.a.	n.a.	n.a.	n.a.	n.a.	
KKI-1	n.a.	n.a.	n.a.	n.a.	n.a.	

<sup>1)</sup>  $Pu_{tot} \leq 8,02$  w/o

<sup>2)</sup> 0,2...0,3 w/o U-235

# MOX - Handling Aspects

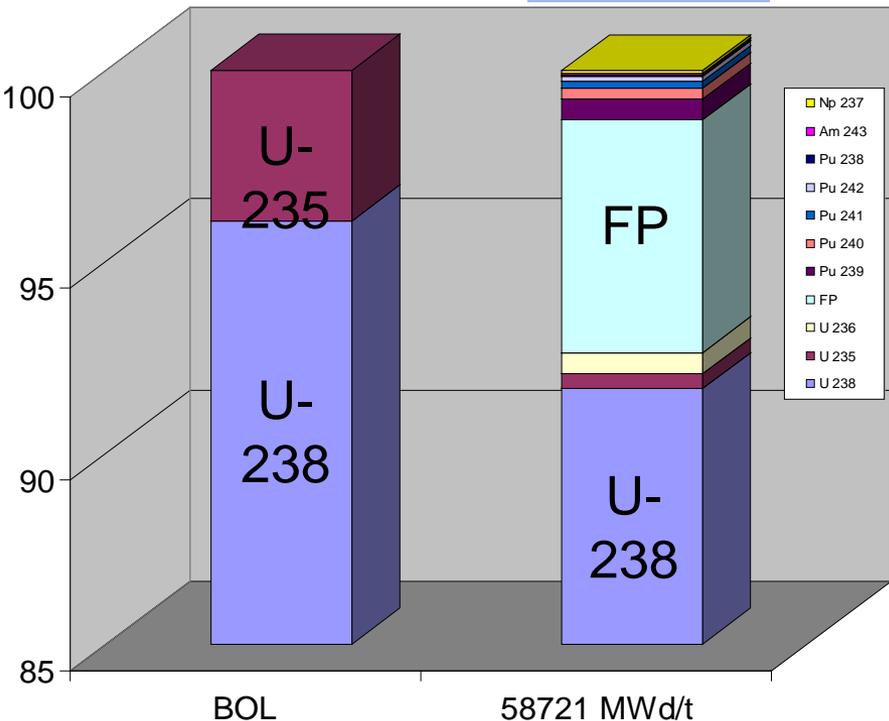
1. Manufacturing
  2. Transport
  3. Receiving inspection
  4. On-site storage
  5. Reactor-physics properties
  6. Safeguards
  7. Post-operation storage
  8. Transport and intermediate storage
- our area of expertise

# MOX - Physical Properties (1): Pu-Balance

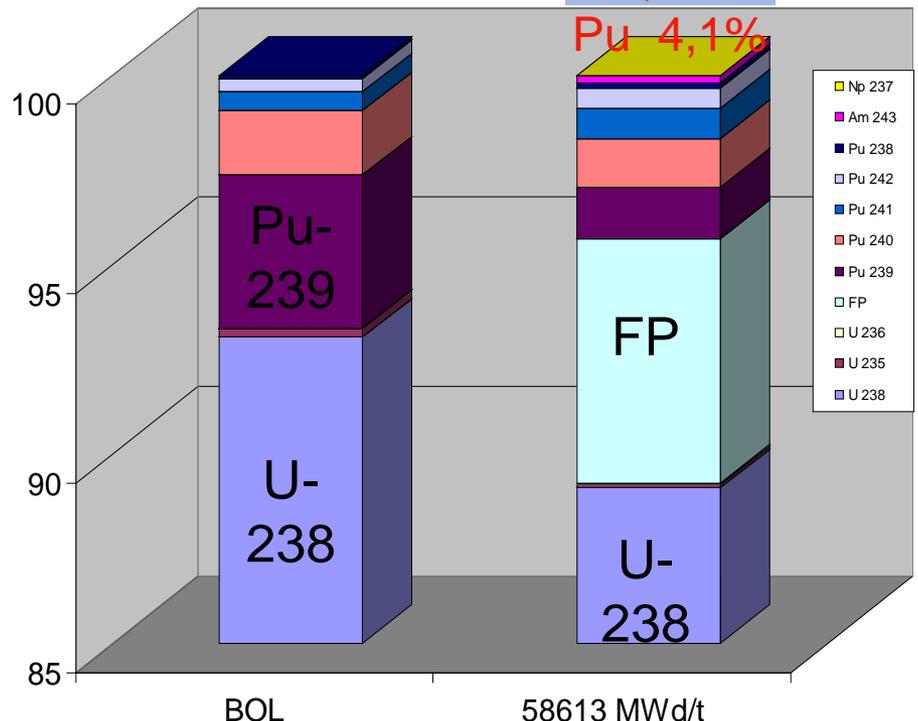
TPu 0,04%  
Pu 1,2%

Pu 6,7%

TPu 0,2%  
Pu 4,1%



Uranium-FA



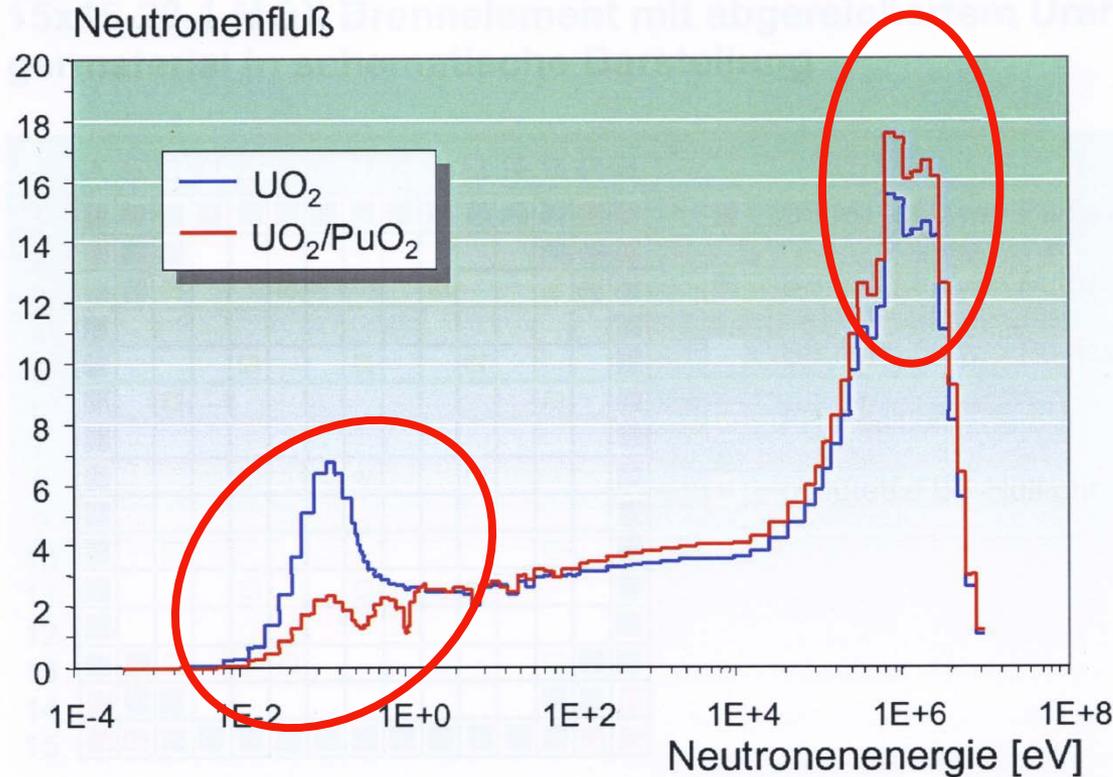
MOX-FA

# MOX - Physical Properties (2): General Overview

	U			Pu					Am
	235	236	238	238	239	240	241	242	241
$\sigma_{f,th} \text{ (b)}$	583				743		1009		
$v_{th}$	2,4				2,9		3,0		
$\beta_{th}$	0,0070				0,0023		0,0055		
<b>E/fission (MeV)</b>	201,7		205		210		212,4		
<b><math>E_{n,max}, E_{avg}</math> (MeV) <sup>1)</sup></b>	0,65/1,95				0,70/2,08		0,67/2,01		
<b>heat (mW/g)</b>				560	1,9	6,8	4,2	0,1	114
<b>surface dose rate 1kg</b>									
<b>n-dose (mSv/h)</b>				640		300,0		310,0	
<b><math>\gamma</math>-dose (mSv/h)</b>				240					27000

1) 
$$\chi_p(E) = \frac{2}{\sqrt{\pi} \left(\frac{2}{3} E_{avg}\right)^{3/2}} \sqrt{E} e^{-E/T}$$

# MOX - Physical Properties (3): PWR n-spectra (U and MOX-core)



Zry-properties

transient  
reaction

# MOX - Physical Properties (4): Consequences

Parameter	Affected Area	Consequence
n-energy hardening	fast fluence in structural materials	irradiation damage (irr.-)
	lower n-absorption	criticality, CRW
	moderator-condition (density, void)	$\Gamma_T$
lower fraction delayed n ( $\beta$ ) transients	faster transient response	
higher fission energy effectively none	less fission-products	
Pu-241, Am-241 manufacturing	heating of unirradiated material	
	dose-rate	transport, inspection
ceramics fuel rod design	heat conductivity, inhomogeneous matrix	

## Practical Aspects of MOX - Handling (1): Delivery

### on-site receiving inspection:

- 1) radiation dose for staff about 50-100 $\mu$ Sv/MOX-FA
- 2) cooling in rack prior to wet-storage (about 1 hour per bundle)

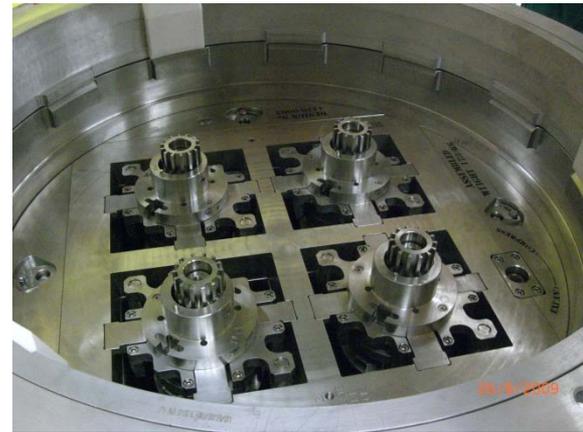
### on site storage of fresh MOX:

only wet-, not dry- storage (capacity)

# Practical Aspects of MOX - Handling (1): Delivery



SIFA (truck) and MX4 (cask)



MX4 loaded with 4 MOX-FA



loading of cooling-rack



cooling-rack

# Practical Aspects of MOX - Handling (2): Reactor

## Physics

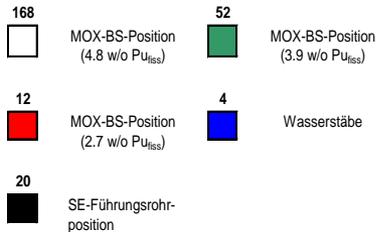
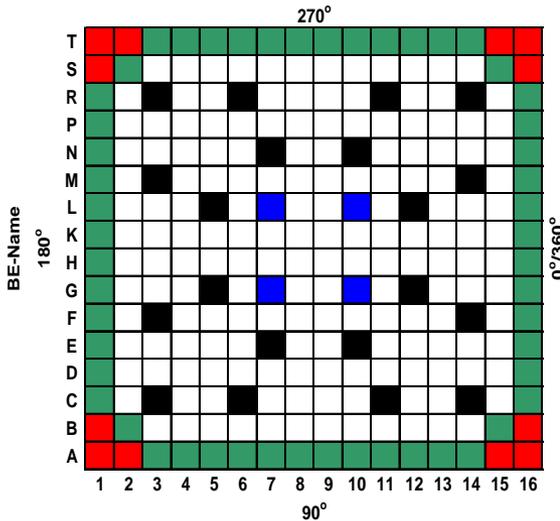
### Reactor-Physics Properties:

1. bundle design (enrichment-levels, water-rods)
2. reactivity versus burnup
3. power-distribution
4. measurement vs. prediction
5. transients and accidents

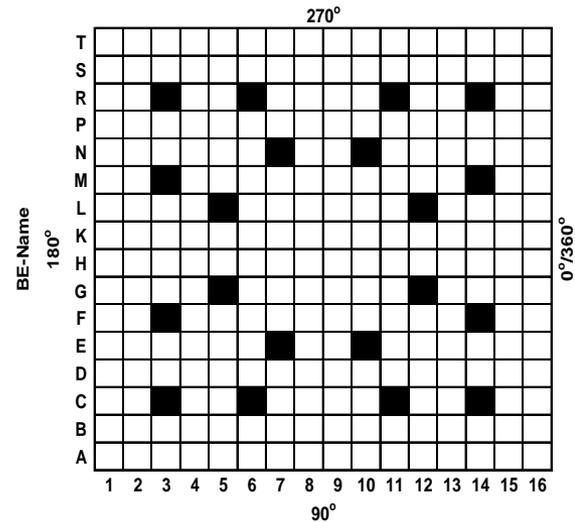
### fuel rod design properties:

1. heat-conductivity
2. fuel temperature
3. fission-gas release

# Practical Aspects of MOX - Handling (2): Bundle Design



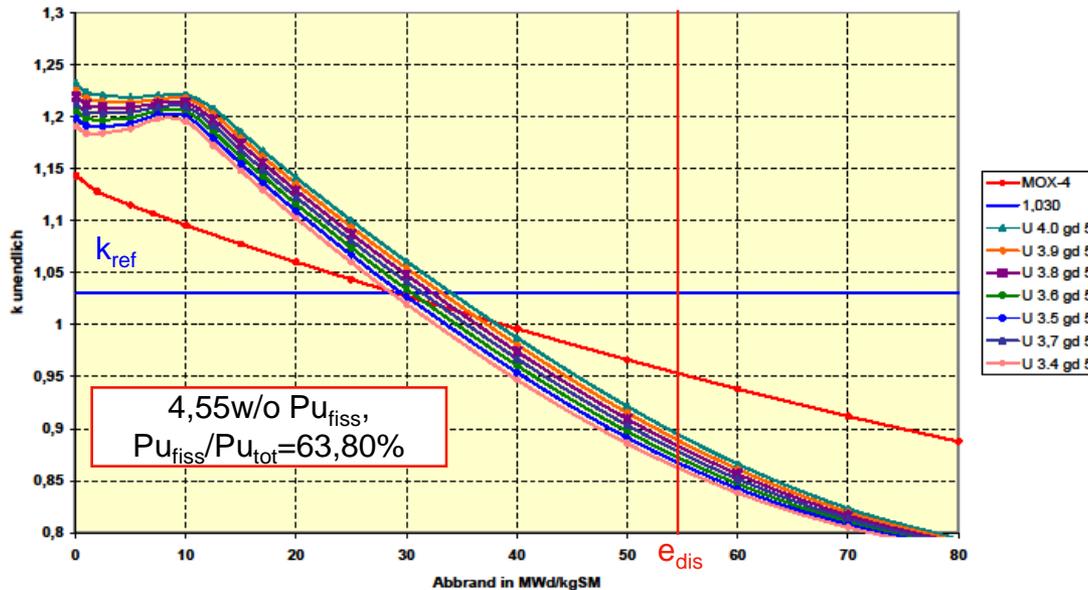
MOX-FA



U-FA

# Practical Aspects of MOX - Handling (2): MOX-Reactivity

$k_{\infty}$  unendlich als Funktion des BE-Abbrandes



Excess reactivity less pronounced – Pu-238, Pu-240, Pu-242  
 reactivity decline slower – in-situ breed&burn of Pu-241

reactivity-equivalence:

$$\int_0^{e_{dis}} k_{\infty}^{(U)}(e) de = \int_0^{e_{dis}} k_{\infty}^{(MOX)}(e) de$$

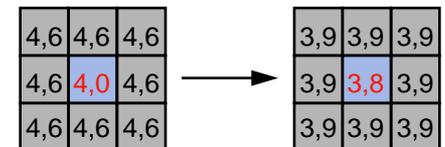
alternative

$$k_{ref} = k_{\infty}^{(U)}(e_0) = k_{\infty}^{(MOX)}(e_0)$$

or:

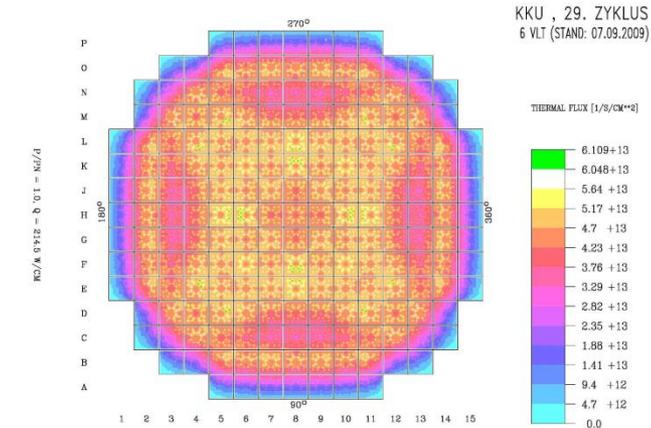
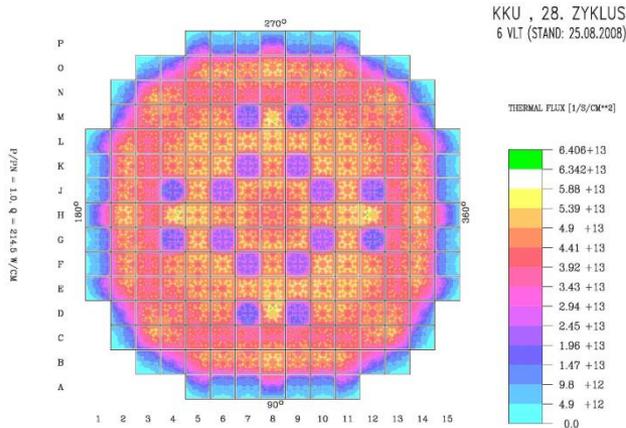
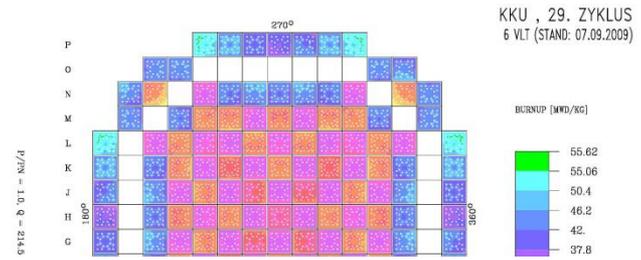
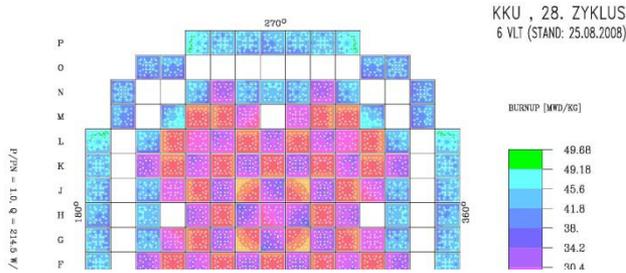
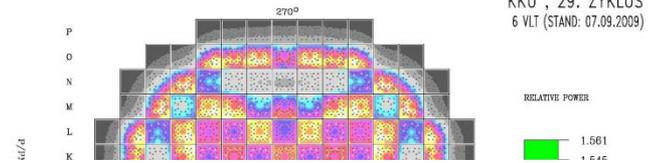
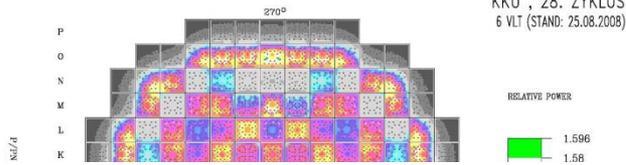
- OECD
- equilibrium-cycles (EKK-study)

Equivalence dependent on surrounding U-235 enr.:



MOX-4 and equivalent U-235 enrichment

# Practical Aspects of MOX - Handling (2): Power Distribution



## Practical Aspects of MOX - Handling (2): Exp. vs Prediction

Accuracy of core-simulator prediction:

1. no influence of MOX loading on difference calculation – aeroball-measurement
2. apparent influence on prediction of critical boron-concentration, but code specific: only AREVAs CASCADE-simulator affected, not e.g. CMS (Studsvik-Scandpower)

# Practical Aspects of MOX - Handling (2): Transients

Most pronounced examples:

1. ATWS: more negative  $\Gamma_T$  helps voiding and reduces heat input at ATWS
2. LOCA: PCT higher in MOX - ECR not limiting in KWU-plants (2 min); core failure rates (German safety criterion) higher in mixed cores;

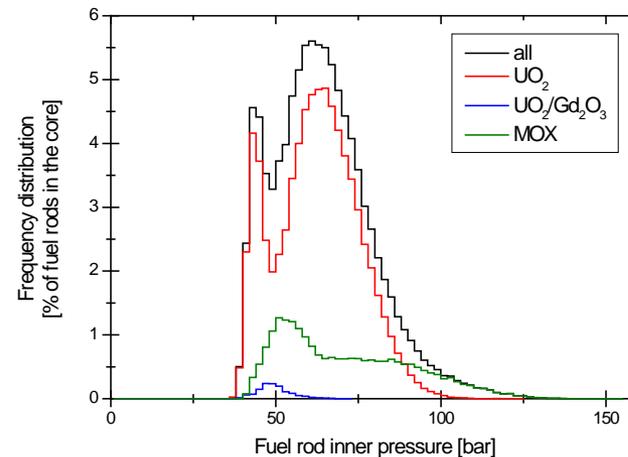
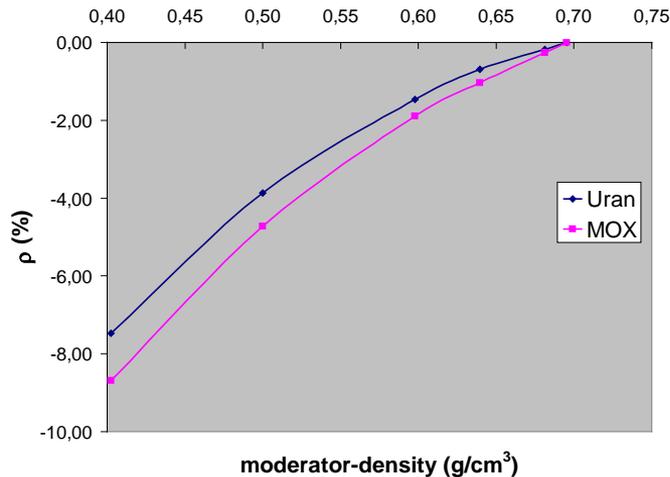
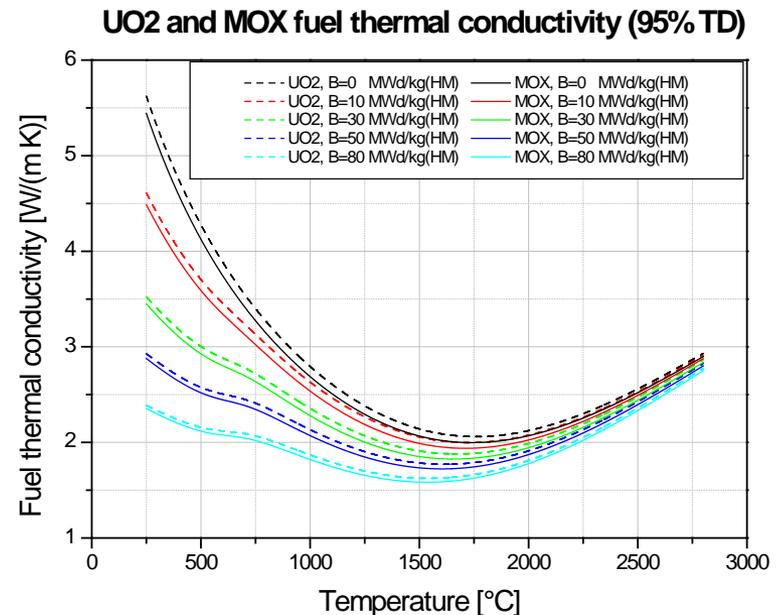


FIG. 5. Resulting distribution of rod internal pressures in the core of a German 16x16 PWR with 45370 FRs containing UO<sub>2</sub>, UO<sub>2</sub>/Gd<sub>2</sub>O<sub>3</sub>, and MOX fuel

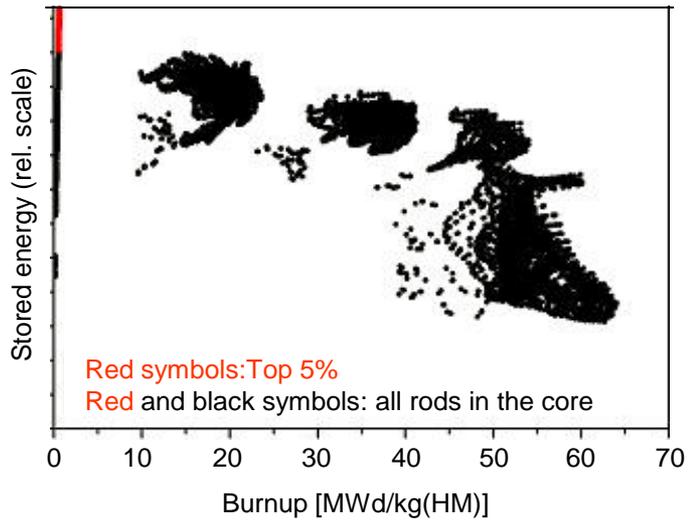
# Practical Aspects of MOX - Handling (2): Fuel-Rod-Design

- heat-conductivity lower
- Pufiss-distribution inhomogenous compared to U-235 nuclei in U-Matrix: >60% proportion of fissile nuclei in PuO microcrystal vs 5% proportion of fissile nuclei in UO2 microcrystal
- more reactivity and power at higher bup (reflecting  $k_{inf}$ (burnup))
- higher fuel temperature
- more fission gas release
- KWU-plants: generally additional lower fuel-rod-plenum!

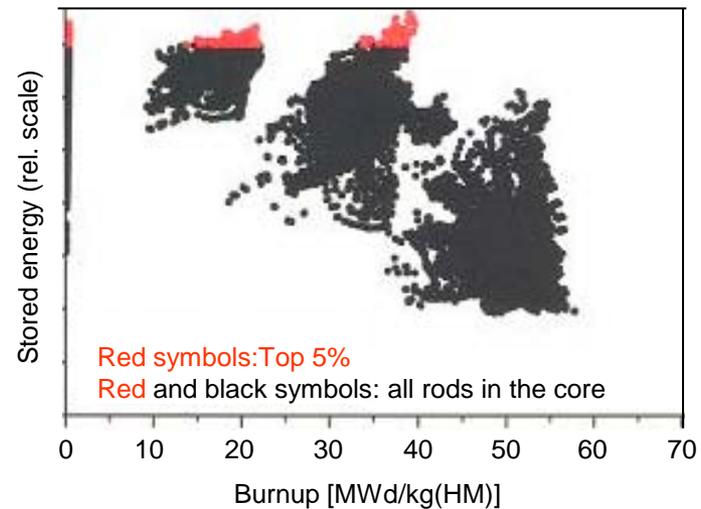


# Practical Aspects of MOX - Handling (2): Fuel-Rod-Design

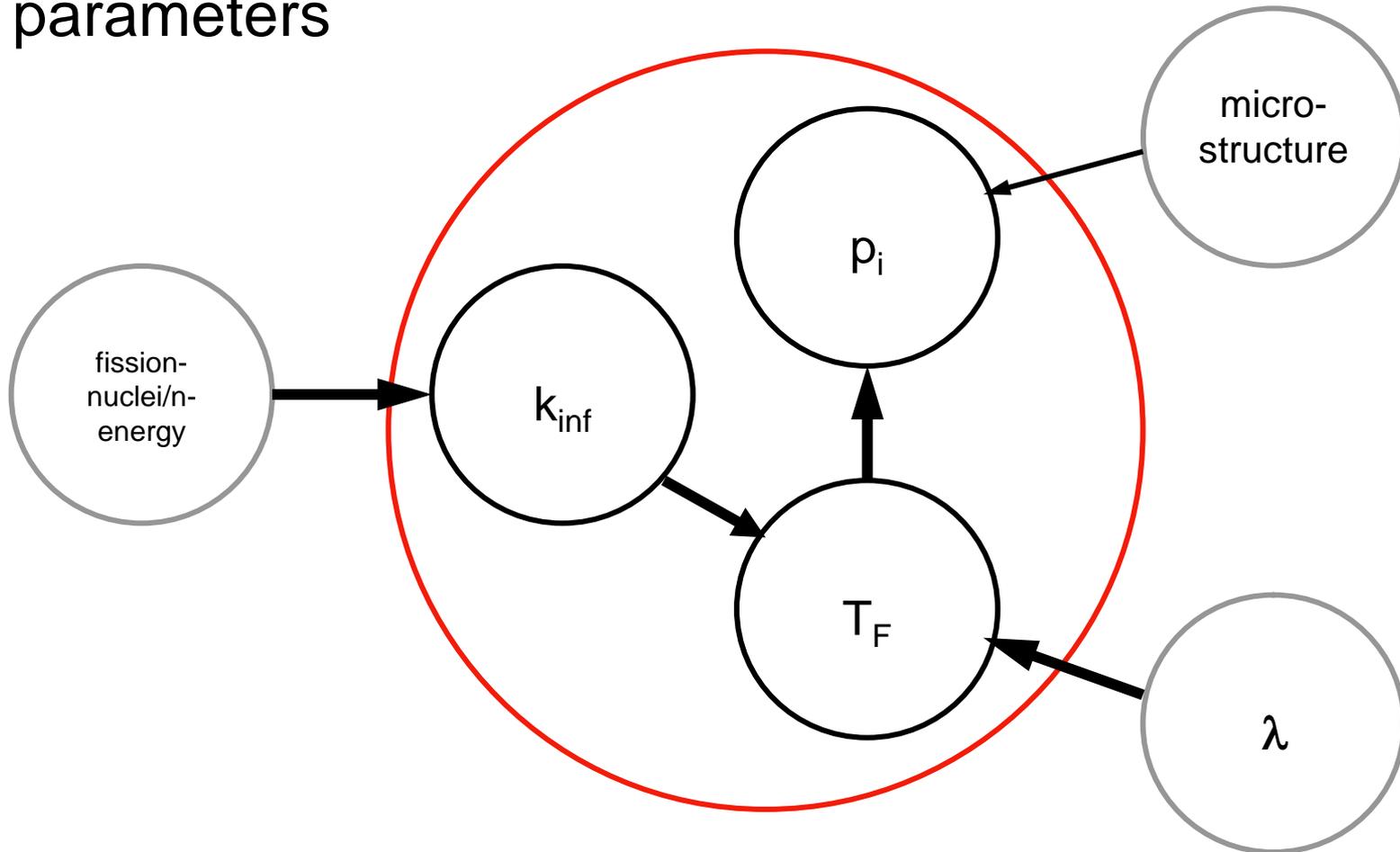
Stored energy in the rods of a UO2 core at BOC



Stored energy in the rods of a MOX/UO2 core at BOC

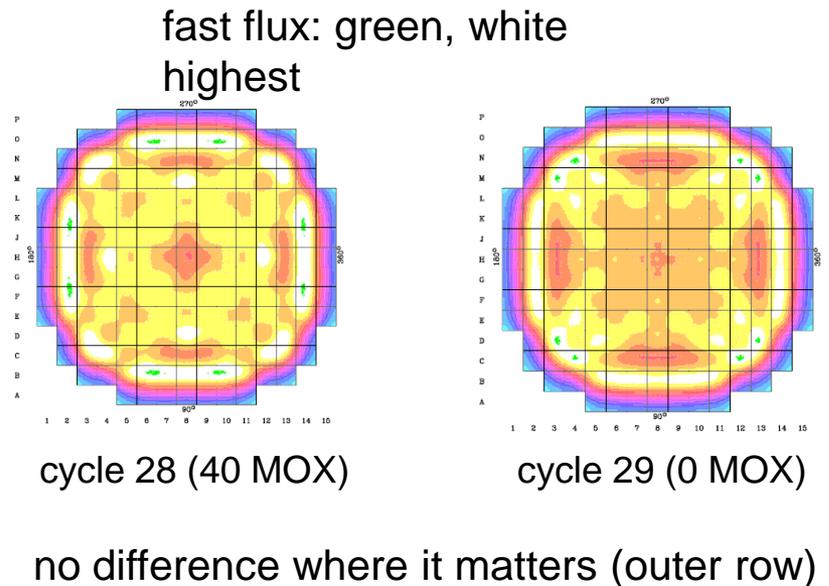
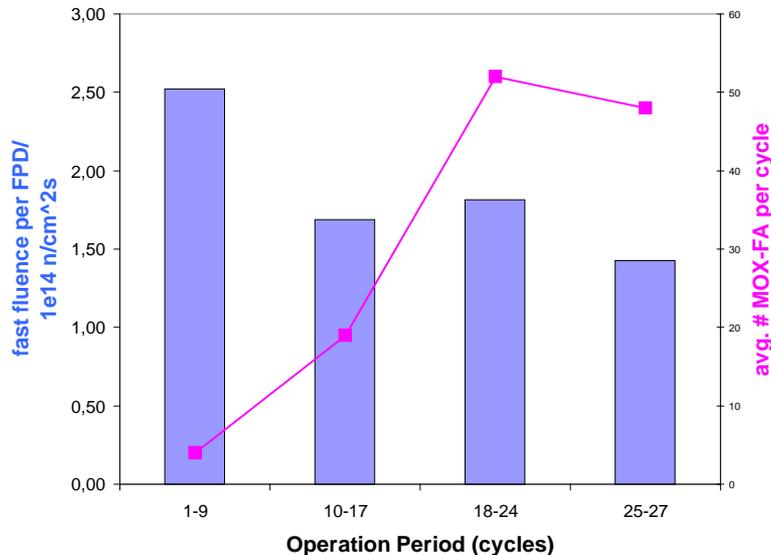


# Practical Aspects of MOX - Handling (2): key parameters



# Practical Aspects of MOX - Handling (3): Fast Fluence

- RPV-Fluence in U- and U/MOX-core: no practical impact of MOX - effect of different loading schemes dominant (in-out-loading vs. out-in)



## Practical Aspects of MOX - Handling (4): CR-worth

- no adaption necessary in KWU-plants
- IFM cold shutdown-criterion easy to meet
- KKKU-example cycle 28 (U/MOX) vs. cycle 29 (U):  
148 ppm B/% $\Delta\rho$  (MOX) vs. 138 ppm B/% $\Delta\rho$

## Practical Aspects of MOX - Handling (5): Safeguards

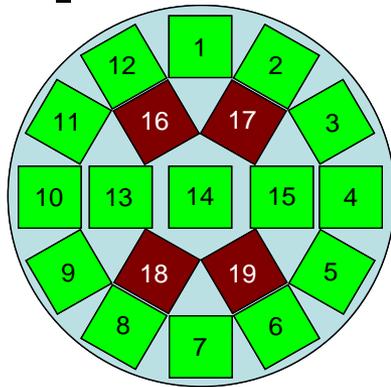
1. camera-surveillance system: additional cameras
2. IAEA inspections: monthly inspections

# Practical Aspects of MOX - Handling (6): Back-End

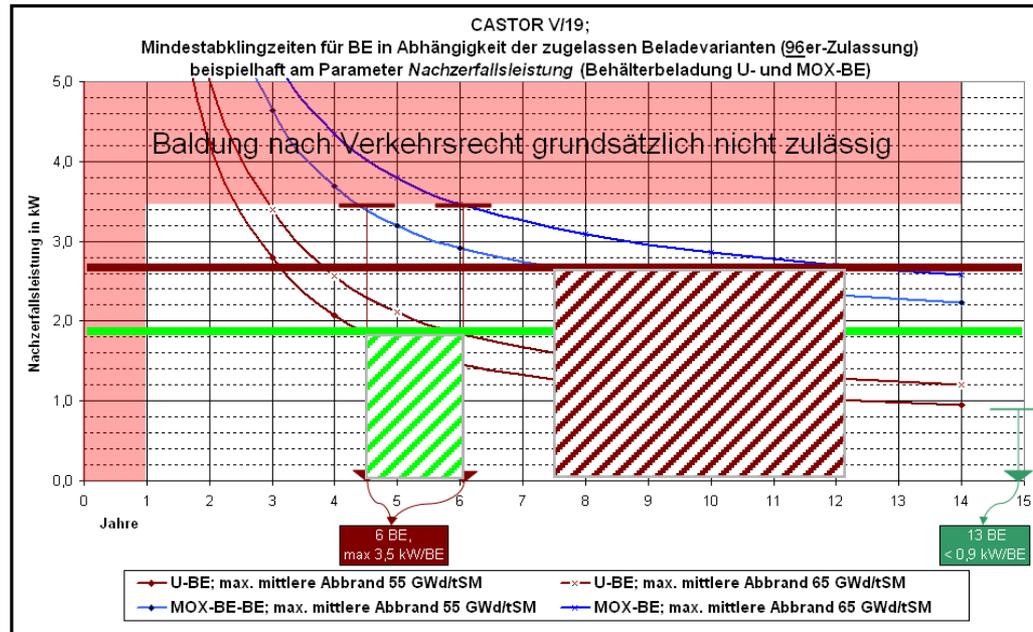
## transport and storage container:

- max 4 MOX-FA out of 19 FA per cask (expected 6 starting in 2012)
- burnup restricted to 55 MWd/kg (U: 65 MWd/kg)
- heat load restriction requires longer storage time: MOX-free cores

EOPL!!!  
today

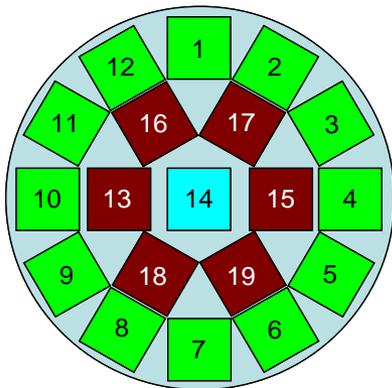


 <2,65 KW  
 <1,83 KW

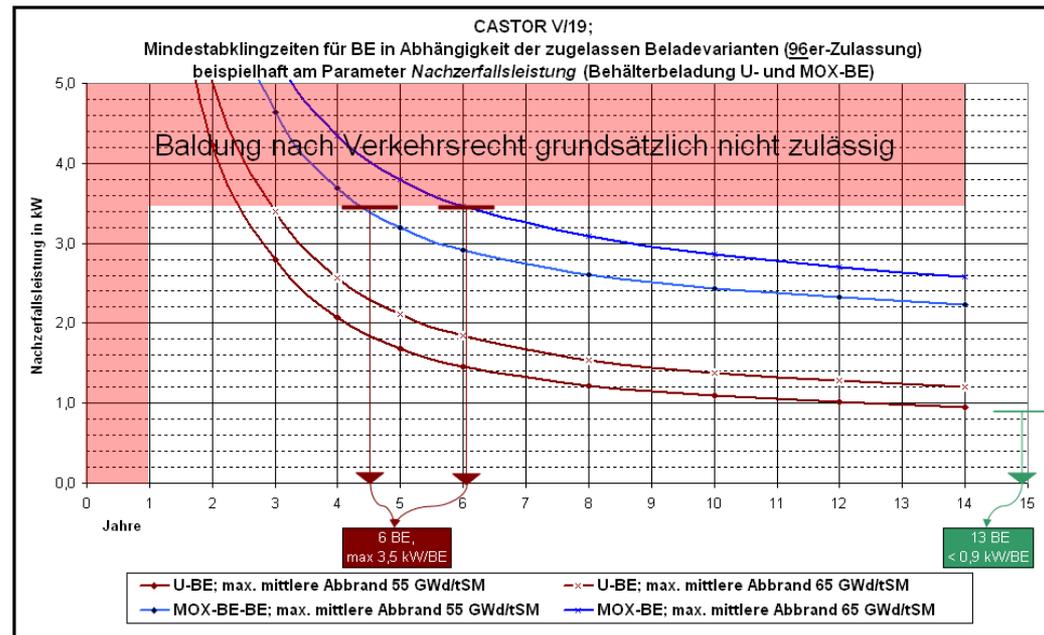


# Practical Aspects of MOX - Handling (6): Back-End

future (a little bit more fortunate):



- <math>< 3,5 \text{ kW} = h\_{\text{MOX}}</math>
- depending on  $h_{\text{MOX}}$
- depending on  $h_{\text{MOX}}$



## Conclusions:

### MOX are ...

- ...more expensive (at least German situation)
- ...more difficult to fabricate
- ...more complicated to handle on-site
- ...more closely supervised by IAEA
- ...more appreciated by IFM-people
- ...in need of longer post-operating storage time
- ...more difficult in intermediate storage period

...than Uranium FA.